

## Herman-Wallis Factors for Higher Overtone Bands: Application to HCl

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Theoretical expressions for the Herman-Wallis factors in terms of the Dunham potential-energy parameters and dipole-moment coefficients were derived for higher overtone bands by the method of computer algebra. These results were applied to an analysis of the vibration-rotational intensities of HCl, leading to a good fit of the data and a dipole-moment function that is improved and extended by comparison with previous results.

### 1. INTRODUCTION

In the past few years, numerous experimental papers have appeared (1-4) reporting accurate vibration-rotational line intensities for higher overtone bands. These data, consisting of the absolute values of the rotationless dipole-moment matrix elements and the corresponding Herman-Wallis coefficients (5, 6), are necessary in order that one can obtain an accurate representation of the dipole-moment function in the vicinity of the equilibrium internuclear separation. However, in order to accomplish this objective, one needs accurate theoretical expressions (or numerical values) for these quantities.

### 2. HERMAN-WALLIS COEFFICIENTS

Theoretical expressions based on the Dunham potential-energy function correct to terms of order  $a_1^6$  have been published (7-9) for vibrational matrix elements for powers of the reduced displacement from the equilibrium internuclear separation,  $x = (R - R_e)/R_e$ , for  $v' = 0-7$ . If one represents the dipole-moment function  $M(x)$  as a truncated series expansion

$$M(x) = \sum_{j=0}^{v'} M_j x^j, \quad (1)$$

one can write

$$\langle 0 | M(x) | v' \rangle = \sum_{j=0}^{v'} M_j \langle 0 | x^j | v' \rangle. \quad (2)$$

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TABLE I

Theoretical Expressions for the Herman-Wallis Coefficients  $C_v^v'$ 

$v' - v$	$C_v^v'$
0	0
1	$\gamma[-4\theta_0] + \left(\frac{v'+v+1}{2}\right)\gamma^2 \left[ \left(-\frac{41}{4} a_1^2 - 15a_1 + 9a_2 - 12\right)\theta_0 + \left(\frac{13}{2} a_1 + \frac{3}{2}\right)\theta_1 - 2\theta_2 \right]$
2	$\gamma \left[ (-a_1 + 3)\theta_0 - 4\theta_1 \right] + \left(\frac{v'+v+1}{3}\right)\gamma^2 \left[ \left(-\frac{333}{32} a_1^3 + \frac{279}{32} a_1^2 + \frac{129}{8} a_1 a_2 + 18 a_1 - \frac{99}{8} a_2 - 5a_3 + 15\right)\theta_0 + \left(-\frac{135}{8} a_1^2 - \frac{111}{4} a_1 + \frac{37}{2} a_2 - 20\right)\theta_1 + \left(\frac{33}{2} a_1 + \frac{9}{2}\right)\theta_2 - 6\theta_3 \right]$
3	$\gamma \left[ \left(-\frac{1}{4} a_1^2 + 2a_1 - \frac{1}{3} a_2 - \frac{8}{3}\right)\mu_0 + (-3a_1 + 3)\mu_1 - 4\mu_2 \right] + \left(\frac{v'+v+1}{4}\right)\gamma^2 \left[ \left(-\frac{363}{64} a_1^4 + \frac{57}{2} a_1^3 + \frac{37}{8} a_1^2 a_2 - 2a_1^2 - 48a_1 a_2 + \frac{3}{4} a_1 a_3 - 20a_1 + \frac{17}{4} a_2^2 + 16a_2 + 14a_3 - \frac{5}{2} a_4 - 20\right)\mu_0 + \left(-\frac{717}{16} a_1^3 - \frac{69}{16} a_1^2 + \frac{283}{4} a_1 a_2 + 17 a_1 - \frac{81}{4} a_2 - \frac{39}{2} a_3 + \frac{45}{2}\right)\mu_1 + \left(-14a_1^2 - 41a_1 + \frac{88}{3} a_2 - \frac{88}{3}\right)\mu_2 + (27a_1 + 9)\mu_3 - 12\mu_4 \right]$
4	$\gamma \left[ \left(-\frac{1}{16} a_1^3 + \frac{15}{16} a_1^2 - \frac{1}{4} a_1 a_2 - 3a_1 + \frac{3}{4} a_2 - \frac{1}{6} a_3 + \frac{5}{2}\right)\rho_0 + \left(-\frac{3}{2} a_1^2 + \frac{7}{2} a_1 - \frac{4}{3} a_2 - \frac{8}{3}\right)\rho_1 + (-5a_1 + 3)\rho_2 - 4\rho_3 \right] + \left(\frac{v'+v+1}{5}\right)\gamma^2 \left[ \left(-\frac{315}{128} a_1^5 + \frac{3525}{128} a_1^4 - \frac{25}{8} a_1^3 a_2 - \frac{405}{8} a_1^3 - \frac{135}{4} a_1^2 a_2 - \frac{55}{48} a_1^2 a_3 - \frac{175}{16} a_1^2 + \frac{75}{8} a_1 a_2^2 + \frac{195}{2} a_1 a_2 + \frac{25}{8} a_1 a_3 + \frac{3}{4} a_1 a_4 + \frac{75}{4} a_1 - \frac{105}{8} a_2 + \frac{3}{4} a_2 a_3 - \frac{75}{4} a_2 - \frac{55}{2} a_3 + \frac{15}{2} a_4\right)$

As is well known (5, 6), these matrix elements alone do not enable one to deduce a unique set of dipole-moment coefficients  $M_j$  because of the uncertainty of the relative signs of the experimental dipole-moment matrix elements. If, in addition, one knows the (approximate) values of the Herman-Wallis coefficients  $C_v^v'$  defined

TABLE I—Continued

$v' - v$	$C_v^{v'}$
	$  \begin{aligned}  & -\frac{7}{4} a_5 + \frac{105}{4} \rho_0 + \left( \frac{-2865}{64} a_1^4 + \frac{3535}{64} a_1^3 + \frac{2365}{48} a_1^2 a_2 + \frac{131}{12} a_1^2 - \frac{1917}{16} a_1 a_2 \right. \\  & - \frac{73}{24} a_1 a_3 - \frac{135}{8} a_1 + 24 a_2^2 + 16 a_2 + \frac{61}{2} a_3 - 12 a_4 - 28 \rho_1 + \left( \frac{-2965}{32} a_1^3 \right. \\  & - \frac{1045}{32} a_1^2 + \frac{3905}{24} a_1 a_2 + \frac{55}{6} a_1 - \frac{225}{8} a_2 - \frac{505}{12} a_3 + \frac{125}{4} \rho_2 + \left( \frac{5}{2} a_1^2 \right. \\  & \left. - \frac{105}{2} a_1 + 40 a_2 - 40 \right) \rho_3 + (35 a_1 + 15) \rho_4 - 20 \rho_5 \Big] \\  5 & \gamma \left[ \left( -\frac{1}{64} a_1^4 + \frac{3}{8} a_1^3 - \frac{1}{8} a_1^2 a_2 - \frac{21}{10} a_1^2 + \frac{9}{10} a_1 a_2 - \frac{11}{60} a_1 a_3 + 4 a_1 - \frac{1}{20} a_2^2 \right. \right. \\  & - \frac{6}{5} a_2 + \frac{2}{5} a_3 - \frac{1}{10} a_4 - \frac{12}{5} \rho_0 + \left( -\frac{5}{8} a_1^3 + \frac{5}{2} a_1^2 - \frac{5}{3} a_1 a_2 - \frac{13}{3} a_1 \right. \\  & + \frac{3}{2} a_2 - \frac{5}{6} a_3 + \frac{5}{2} \rho_1 + \left( -\frac{15}{4} a_1^2 + 5 a_1 - \frac{7}{3} a_2 - \frac{8}{3} \right) \rho_2 + (-7 a_1 + 3) \rho_3 \\  & \left. \left. - 4 \rho_4 \right) + \left( \frac{v'+v+1}{6} \right) \gamma^2 \left[ \left( -\frac{1935}{2048} a_1^6 + \frac{585}{32} a_1^5 - \frac{2271}{512} a_1^4 a_2 - \frac{297}{4} a_1^4 + \frac{9}{16} a_1^3 a_2 \right. \right. \\  & - \frac{337}{64} a_1^3 a_3 + \frac{285}{4} a_1^3 + \frac{891}{128} a_1^2 a_2^2 + \frac{441}{4} a_1^2 a_2 + \frac{57}{16} a_1^2 a_3 + \frac{3}{160} a_1^2 a_4 \\  & + \frac{117}{4} a_1^2 - \frac{171}{4} a_1 a_2^2 + \frac{629}{80} a_1 a_2 a_3 - 165 a_1 a_2 - \frac{69}{4} a_1 a_3 + \frac{27}{40} a_1 a_4 \\  & + \frac{3}{10} a_1 a_5 - \frac{63}{5} a_1 + \frac{51}{32} a_2^3 + 27 a_2^2 + \frac{3}{10} a_2 a_3 + \frac{9}{8} a_2 a_4 + \frac{99}{5} a_2 - \frac{23}{12} a_3^2 + 46 a_3 \\  & - \frac{153}{10} a_4 + \frac{27}{5} a_5 - \frac{7}{5} a_6 - \frac{168}{5} \rho_0 + \left( -\frac{7857}{256} a_1^5 + \frac{22143}{256} a_1^4 - \frac{277}{32} a_1^3 a_2 \right. \\  & - \frac{6119}{80} a_1^3 - \frac{21873}{160} a_1^2 a_2 - \frac{171}{20} a_1^2 a_3 - \frac{951}{32} a_1^2 + \frac{6343}{80} a_1 a_2^2 + \frac{3503}{20} a_1 a_2 \\  & \left. \left. + \frac{2137}{160} a_1 a_3 + \frac{111}{80} a_1 a_4 + \frac{54}{5} a_1 - \frac{549}{16} a_2^2 + \frac{65}{24} a_2 a_3 - \frac{145}{8} a_2 - \frac{160}{3} a_3 \right) \right]  \end{aligned}  $
	by

$$F_v^v(m) = \langle vJ|M(x)|v'J'\rangle^2 / \langle v0|M(x)|v'0\rangle^2 = 1 + C_v^v m + D_v^v m^2 + \dots, \quad (3)$$

in which  $m = 1/2[J'(J'+1) - J(J+1)]$  and  $v, J$  denote the standard vibrational and rotational quantum numbers, respectively, one can determine the coefficients  $M_j$  unambiguously (6).

TABLE I—Continued

$v' - v$	$C_v^{v'}$
	$  \begin{aligned}  & + \frac{285}{16} a_4 - 10a_5 + 35) \epsilon_1 + \left( \frac{-4389}{32} a_1^4 + \frac{2361}{32} a_1^3 + \frac{373}{2} a_1^2 a_2 + \frac{131}{5} a_1^2 \right. \\  & - \frac{8967}{40} a_1 a_2 - \frac{997}{40} a_1 a_3 - \frac{27}{4} a_1 + \frac{551}{10} a_2^2 + \frac{62}{5} a_2 + \frac{537}{10} a_3 - \frac{531}{20} a_4 \\  & - \frac{186}{5} \epsilon_2 + \left[ \frac{-4575}{32} a_1^3 - \frac{2475}{32} a_1^2 + \frac{2361}{8} a_1 a_2 - \frac{15}{2} a_1 - \frac{279}{8} a_2 - \frac{295}{4} a_3 \right. \\  & \left. + \frac{165}{4} \epsilon_3 + \left( \frac{135}{4} a_1^2 - 60a_1 + 49a_2 - 52 \right) \epsilon_4 + \left( \frac{75}{2} a_1 + \frac{45}{2} \right) \epsilon_5 - 30\epsilon_6 \right] \\  6 & \gamma \left[ \left( -\frac{1}{256} a_1^5 + \frac{35}{256} a_1^4 - \frac{5}{96} a_1^3 a_2 - \frac{7}{6} a_1^3 + \frac{21}{32} a_1^2 a_2 - \frac{1}{8} a_1^2 a_3 + \frac{15}{4} a_1^2 \right. \right. \\  & - \frac{1}{16} a_1 a_2^2 - 2a_1 a_2 + \frac{5}{8} a_1 a_3 - \frac{3}{20} a_1 a_4 - 5a_1 + \frac{3}{16} a_2^2 - \frac{1}{15} a_2 a_3 + \frac{5}{3} a_2 \\  & - \frac{2}{3} a_3 + \frac{1}{4} a_4 - \frac{1}{15} a_5 + \frac{7}{3} \delta_0 + \left( -\frac{15}{64} a_1^4 + \frac{45}{32} a_1^3 - \frac{5}{4} a_1^2 a_2 - \frac{41}{10} a_1^2 \right. \\  & + \frac{101}{40} a_1 a_2 - \frac{27}{20} a_1 a_3 + \frac{21}{4} a_1 - \frac{23}{60} a_2^2 - \frac{28}{15} a_2 + \frac{9}{10} a_3 - \frac{3}{5} a_4 - \frac{12}{5} \delta_1 \\  & + \left( -\frac{35}{16} a_1^3 + \frac{77}{16} a_1^2 - \frac{49}{12} a_1 a_2 - \frac{17}{3} a_1 + \frac{9}{4} a_2 - \frac{3}{2} a_3 + \frac{5}{2} \right) \delta_2 + (-7a_1^2 \\  & \left. \left. + \frac{13}{2} a_1 - \frac{10}{3} a_2 - \frac{8}{3} \right) \delta_3 + (-9a_1 + 3) \delta_4 - 4\delta_5 \right]  \end{aligned}  $

In extending the Dunham formalism by means of computer algebra (10, 11), we have recently obtained extensive new results (correct to higher powers of  $a_1$ ) for the energy term-value coefficients  $Y_{kl}$ , wavefunctions, expectation values, and vibration-rotational matrix elements of  $x^l$ ; these will be published elsewhere (11, 12). Here we report theoretical expressions for the Herman-Wallis coefficients  $C_v^{v'}$  and  $D_v^{v'}$  for  $0 \leq (v' - v) \leq 6$ , correct through terms of order  $a_1^6$ . Some of these results are new (the correction term proportional to  $\gamma^2$  ( $\gamma = 2B_e/\omega_e$ ) in  $C_v^{v+5}$  and the  $(v' - v) = 6$  results); in addition, as a result of the present work, a few minor misprints and mistakes<sup>2</sup> have been detected in published expressions (13, 14). For convenience we list in Tables I and II all the results for  $C_v^{v'}$  and  $D_v^{v'}$  expressed in terms of the notation

<sup>2</sup> The coefficient of  $\gamma^2 \phi_0 a_1 a_2$  in Ref. (13) should read 129/8 not 127/8; the coefficients of  $\gamma^2 \rho_0 a_1^5$ ,  $\gamma^2 \rho_0 a_1 a_4$ , and  $\gamma^2 \rho_1 a_4$  in Ref. (14) should read  $-63/32$ ,  $3/5$ , and  $-6$ , respectively, not  $63/32$ ,  $1/10$ , and  $-45/8$ .

TABLE II

Theoretical Expressions for the Herman-Wallis Coefficients  $D_v^v'$ 

$v' - v$	$D_v^v'$
0	$\gamma^2 [2v_1]$
1	$(\frac{1}{2} C_v^{v+1})^2 + \gamma^2 \left[ \left( -\frac{3}{2} a_1 - \frac{3}{2} \right) \theta_1 + 4\theta_2 \right]$
2	$(\frac{1}{2} C_v^{v+2})^2 + \gamma^2 \left[ 4\theta_0 + \left( -\frac{9}{2} a_1^2 - \frac{9}{2} a_1 + 4a_2 - 4 \right) \theta_1 + (-a_1 - 3) \theta_2 + 6\theta_3 \right]$
3	$(\frac{1}{2} C_v^{v+3})^2 + \gamma^2 \left[ (2a_1 - 6) \mu_0 + \left( \frac{-99}{32} a_1^3 - \frac{99}{32} a_1^2 + \frac{3}{8} a_1 a_2 - 3a_1 - \frac{21}{8} a_2 \right. \right.$ $\left. \left. + \frac{5}{2} a_3 + \frac{13}{2} \right) \mu_1 + \left( -\frac{39}{4} a_1^2 - \frac{21}{2} a_1 + 9a_2 - 8 \right) \mu_2 + \left( \frac{3}{2} a_1 - \frac{9}{2} \right) \mu_3 + 8\mu_4 \right]$
4	$(\frac{1}{2} C_v^{v+4})^2 + \gamma^2 \left[ \left( \frac{3}{4} a_1^2 - \frac{11}{2} a_1 + \frac{2}{3} a_2 + \frac{91}{12} \right) \rho_0 + \left( -\frac{3}{2} a_1^4 - \frac{3}{2} a_1^3 - 3a_1^2 a_2 - \frac{3}{2} a_1^2 - \frac{9}{2} a_1 a_2 + \frac{1}{2} a_1 a_3 + \frac{13}{2} a_1 + 2a_2^2 - 2a_2 - 2a_3 + 2a_4 - 8 \right) \rho_1 + \left( -11 a_1^3 \right. \right.$ $\left. \left. - \frac{45}{4} a_1^2 + 5a_1 a_2 - 10a_1 - 6a_2 + \frac{17}{3} a_3 + 9 \right) \rho_2 + \left( -\frac{57}{4} a_1^2 - 18 a_1 \right. \right.$ $\left. \left. + 15a_2 - 12 \right) \rho_3 + \left( 6a_1 - 6 \right) \rho_4 + 10\rho_5 \right]$
5	$(\frac{1}{2} C_v^{v+5})^2 + \gamma^2 \left[ \left( \frac{1}{4} a_1^3 - \frac{13}{4} a_1^2 + \frac{2}{3} a_1 a_2 + \frac{31}{3} a_1 - 2a_2 + \frac{1}{3} a_3 - 9 \right) \epsilon_0 \right. \right.$ $\left. \left. + \left( -\frac{315}{512} a_1^5 - \frac{315}{512} a_1^4 - \frac{215}{64} a_1^3 a_2 - \frac{5}{8} a_1^3 - \frac{255}{64} a_1^2 a_2 - \frac{93}{32} a_1^2 a_3 + \frac{65}{16} a_1^2 \right. \right. \right.$ $\left. \left. \left. + \frac{41}{32} a_1 a_2^2 - \frac{5}{2} a_1 a_2 - \frac{143}{32} a_1 a_3 + \frac{17}{16} a_1 a_4 - \frac{45}{4} a_1 - \frac{39}{32} a_2^2 + \frac{37}{12} a_2 a_3 \right. \right. \right. \right.$ $\left. \left. \left. + \frac{35}{12} a_2 - \frac{11}{6} a_3 - \frac{27}{16} a_4 + \frac{7}{4} a_5 + \frac{28}{3} \right) \epsilon_1 + \left( \frac{-505}{64} a_1^4 - \frac{255}{32} a_1^3 - \frac{13}{2} a_1^2 a_2 \right. \right. \right. \right]$

TABLE II—Continued

$v' - v$	$D_v^{v'}$
	$  \begin{aligned}  & -\frac{15}{2} a_1^2 - \frac{117}{8} a_1 a_2 + \frac{47}{12} a_1 a_3 + \frac{27}{2} a_1 + \frac{25}{4} a_2^2 - 6a_2 - \frac{9}{2} a_3 + \frac{9}{2} a_4 \\  & - 10\epsilon_2 + \left( \frac{-759}{32} a_1^3 - \frac{819}{32} a_1^2 + \frac{123}{8} a_1 a_2 - 21a_1 - \frac{81}{8} a_2 + \frac{19}{2} a_3 + \frac{23}{2} \right) \epsilon_3 \\  & + \left( -\frac{33}{2} a_1^2 - 27a_1 + 22a_2 - 16 \right) \epsilon_4 + \left( \frac{25}{2} a_1 - \frac{15}{2} \right) \epsilon_5 + 12\epsilon_6 \Big] \\  6 & \left( \frac{1}{2} C_v^{v+6} \right)^2 + \gamma^2 \left[ \left( \frac{5}{64} a_1^4 - \frac{25}{16} a_1^3 + \frac{5}{12} a_1^2 a_2 + \frac{4051}{480} a_1^2 - \frac{173}{60} a_1 a_2 + \frac{9}{20} a_1 a_3 \right. \right. \\  & - \frac{197}{12} a_1 + \frac{23}{180} a_2^2 + \frac{1429}{360} a_2 - \frac{21}{20} a_3 + \frac{1}{5} a_4 + \frac{1859}{180} \delta_0 + \left( \frac{-117}{512} a_1^6 \right. \\  & - \frac{117}{512} a_1^5 - \frac{75}{32} a_1^4 a_2 - \frac{15}{64} a_1^4 - \frac{165}{64} a_1^3 a_2 - \frac{137}{32} a_1^3 a_3 + \frac{65}{32} a_1^3 - \frac{21}{32} a_1^2 a_2^2 \\  & - \frac{15}{8} a_1^2 a_2 - \frac{81}{16} a_1^2 a_3 - \frac{99}{40} a_1^2 a_4 - \frac{75}{8} a_1^2 - \frac{81}{32} a_1 a_2^2 + \frac{111}{40} a_1 a_2 a_3 + \frac{35}{8} a_1 a_2 \\  & - 3a_1 a_3 - \frac{189}{40} a_1 a_4 + \frac{33}{20} a_1 a_5 + \frac{691}{40} a_1 + \frac{3}{4} a_2^3 - \frac{3}{4} a_2^2 - \frac{21}{10} a_2 a_3 + 3a_2 a_4 \\  & - \frac{47}{10} a_2 + a_3^2 + 2a_3 - \frac{9}{5} a_4 - \frac{3}{2} a_5 + \frac{8}{5} a_6 - \frac{53}{5} \delta_1 + \left( \frac{-1149}{256} a_1^5 - \frac{1155}{256} a_1^4 \right. \\  & - \frac{417}{32} a_1^3 a_2 - \frac{35}{8} a_1^3 - \frac{567}{32} a_1^2 a_2 - \frac{93}{16} a_1^2 a_3 + \frac{189}{16} a_1^2 + \frac{111}{16} a_1 a_2^2 \\  & - \frac{21}{2} a_1 a_2 - \frac{105}{8} a_1 a_3 + \frac{93}{20} a_1 a_4 - 19a_1 - \frac{63}{16} a_2^2 + \frac{183}{20} a_2 a_3 + \frac{77}{12} a_2 \\  & - 5a_3 - \frac{15}{4} a_4 + \frac{39}{10} a_5 + \frac{133}{12} \delta_2 + \left( \frac{-2919}{128} a_1^4 - \frac{189}{8} a_1^3 - \frac{105}{16} a_1^2 a_2 \right. \\  & - 21a_1^2 - \frac{63}{2} a_1 a_2 + \frac{45}{4} a_1 a_3 + 23a_1 + \frac{105}{8} a_2^2 - 12a_2 - \frac{15}{2} a_3 + \frac{15}{2} a_4 \\  & - 12\delta_3 + \left( \frac{-161}{4} a_1^3 - \frac{189}{4} a_1^2 + 33 a_1 a_2 - 36a_1 - 15a_2 + 14a_3 + 14 \right) \delta_4 \\  & \left. + \left( -15a_1^2 - \frac{75}{2} a_1 + 30a_2 - 20 \right) \delta_5 + (21a_1 - 9) \delta_6 + 14\delta_7 \right]  \end{aligned}  $

TABLE III

Experimental Potential-Energy Parameters and Rotationless Dipole-Moment Matrix Elements

j	$a_j$	$\langle 0   M(x)   j \rangle / \text{Debye}$
1	$-2.3633725 \pm 3.5 \times 10^{-5}$	$7.12 \times 10^{-2} \pm 2.5 \times 10^{-3}$
2	$3.6605756 \pm 1.9 \times 10^{-4}$	$-7.75 \times 10^{-3} \pm 2.5 \times 10^{-4}$
3	$-4.74921 \pm 1.3 \times 10^{-3}$	$5.15 \times 10^{-4} \pm 2.0 \times 10^{-5}$
4	$5.4529 \pm 9.9 \times 10^{-3}$	$-3.063 \times 10^{-5} \pm 1.0 \times 10^{-7}$
5	$-5.516 \pm 3.2 \times 10^{-2}$	$-8.42 \times 10^{-6} \pm 3.6 \times 10^{-8}$
6	$4.284 \pm 0.13$	$6.61 \times 10^{-6} \pm 2.4 \times 10^{-8}$
	$\gamma = 7.083694 \times 10^{-3} \pm 1.7 \times 10^{-8}$	$\langle 0   M(x)   0 \rangle = 1.10847 \pm 5 \times 10^{-4}$

$$\begin{aligned}
\nu_j &= M_j / \langle 0 | M(x) | 0 \rangle, \\
\theta_j &= \sqrt{\gamma} M_j / \sqrt{2} \langle 0 | M(x) | 1 \rangle, \\
\phi_j &= \gamma M_j / \sqrt{2} \langle 0 | M(x) | 2 \rangle, \\
\mu_j &= \gamma^{3/2} \sqrt{3} M_j / 2 \langle 0 | M(x) | 3 \rangle, \\
\rho_j &= \gamma^2 \sqrt{6} M_j / 2 \langle 0 | M(x) | 4 \rangle, \\
\epsilon_j &= \gamma^{5/2} \sqrt{15} M_j / 2 \langle 0 | M(x) | 5 \rangle, \\
\delta_j &= 3\gamma^3 \sqrt{5} M_j / 2 \langle 0 | M(x) | 6 \rangle. \tag{4}
\end{aligned}$$

Because of the form of these expressions a large amount of cancellation can occur in determining both the individual coefficients of  $M_j$  and the final numerical values. Consequently, in order to obtain consistent results, one must retain all the contributions to the same power of  $\gamma$ . For this reason, the correction term to  $C_v^{v+6}$  is not given because it contains contributions of the order of  $a_1^7$ . Finally, higher-order corrections (higher powers of  $\gamma$ ) to the  $C$  and  $D$  coefficients, as well as the coefficients of  $m^3$ ,  $m^4$ , etc., in Eq. [3] can be derived by identical methods. Such extensions, however, are not warranted at present in light of the accuracy of the experimental results.

### 3. APPLICATION TO HCl

As an example to illustrate the use of the Herman-Wallis coefficients in extracting the dipole-moment coefficients  $M_j$  from the experimental data, we have reanalyzed (15) the vibration-rotational intensities of HCl incorporating both the recent results

TABLE IV  
Coefficients of the Dipole-Moment Function

$j$	$M_j/\text{Debye}$
0	$1.09333 \pm 8.6 \times 10^{-4}$
1	$1.20538 \pm 0.039$
2	$0.03842 \pm 0.060$
3	$-1.4882 \pm 0.10$
4	$-0.9881 \pm 0.14$
5	$-0.6476 \pm 0.19$
6	$-0.9358 \pm 0.41$

for the higher overtone bands (4) and the accurate Dunham potential-energy parameters obtained from a global analysis of the transition frequencies (16). These data are assembled in Table III, including estimates of the experimental uncertainties

TABLE V  
Comparison of Calculated and Measured Herman-Wallis Coefficients

	Experiment	Theory
$C_0^0$	-	0
$D_0^0$	-	$1.1 \times 10^{-4} \pm 3.7 \times 10^{-6}$
$C_0^1$	$-2.60 \times 10^{-2} \pm 2.0 \times 10^{-3}$	$-2.66 \times 10^{-2} \pm 9.3 \times 10^{-4}$
$D_0^1$	$4.5 \times 10^{-4} \pm 2.0 \times 10^{-4}$	$2.8 \times 10^{-4} \pm 7.7 \times 10^{-6}$
$C_0^2$	$-8.60 \times 10^{-3} \pm 1.5 \times 10^{-3}$	$-5.67 \times 10^{-3} \pm 7.9 \times 10^{-4}$
$D_0^2$	$4.1 \times 10^{-4} \pm 2.0 \times 10^{-4}$	$3.1 \times 10^{-4} \pm 8.5 \times 10^{-6}$
$C_0^3$	$1.70 \times 10^{-2}$	$1.07 \times 10^{-2} \pm 2.2 \times 10^{-3}$
$D_0^3$	-	$3.7 \times 10^{-4} \pm 1.7 \times 10^{-5}$
$C_0^4$	$2.77 \times 10^{-2} \pm 1.1 \times 10^{-3}$	$1.20 \times 10^{-2} \pm 7.3 \times 10^{-3}$
$D_0^4$	$1.42 \times 10^{-3} \pm 1.7 \times 10^{-4}$	$7.9 \times 10^{-4} \pm 2.5 \times 10^{-5}$
$C_0^5$	$1.74 \times 10^{-2} \pm 1.3 \times 10^{-3}$	$3.21 \times 10^{-2} \pm 7.0 \times 10^{-3}$
$D_0^5$	$4.61 \times 10^{-4} \pm 2.4 \times 10^{-4}$	$1.4 \times 10^{-3} \pm 3.2 \times 10^{-5}$
$C_0^6$	$3.35 \times 10^{-2} \pm 1.1 \times 10^{-3}$	$4.99 \times 10^{-2} \pm 2.9 \times 10^{-3}$
$D_0^6$	$7.99 \times 10^{-4} \pm 1.8 \times 10^{-4}$	$1.3 \times 10^{-3} \pm 1.8 \times 10^{-5}$

(4, 13, 16, 17). With the choice of signs for the dipole-moment matrix elements indicated in Table III, we obtained the best overall fit. The corresponding theoretical values of the dipole-moment and Herman-Wallis coefficients are given in Tables IV and V. The accompanying error estimates were obtained by a Monte-Carlo sampling method, according to which the input parameters ( $a_j$ ,  $\gamma$ , and  $\langle 0|M(x)|v' \rangle$ ) were subjected to random variation within one (nominal) standard deviation of their published values, and the variation of the  $M_j$ ,  $C_0^{v'}$ , and  $D_0^{v'}$  coefficients correspondingly determined. These estimates are equivalent to one standard deviation, and thus are indicative of the relative uncertainties. A detailed comparison of the present results with the previous analysis (15) based on  $0 \leq v' \leq 5$  demonstrates that the addition of the  $6 \leftarrow 0$  results and the improved potential-energy parameters improves the overall fit; all the  $C$  and  $D$  coefficients have the correct signs and approximately the correct magnitudes. We are thus led to believe that the present dipole-moment function is correspondingly better.

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